

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Patent Application of Manabu KOBAYASHI, et al.

Application No.: 10/583,154

Filed: June 16, 2006

For: LUBRICANT BASE OIL AND METHOD OF PRODUCING THE SAME

Group Art Unit: 1797

Examiner: Chantel Graham

Confirmation No.: 2556

DECLARATION UNDER 37 C.F.R. § 1.132

I, Manabu Kobayashi, declare that:

I am one of the inventors of the above-captioned patent application.

I received my Master of Engineering from University of Tokyo in 1994, and have been employed by Japan Energy Corporation since 1994, where I have been engaged mainly in research and development of hydrotreating and hydrocracking process and catalysts. I also received my Doctor of Engineering from Shinshu University in 2009.

I have made the following experiments in order to evaluate a molecular structure of lubricant base oil produced by hydrocracking of Fischer-Tropsh waxes, which mainly consists of isoparaffin. I and the other inventors evaluated the influence of the branching numbers (Nb) and carbon numbers (Nc) of isoparaffin formed on the viscosity properties. As a result, we found that there is a suitable range of Nb and Nc to maximize viscosity properties, especially viscosity index of the lubricant base oil composed mainly of isoparaffins. We firmly believe this finding will be a key technology for producing lubricant base oils of extremely high performance.

Experimental Procedure

(Additional Comparative Example A1)

The same starting wax A and catalyst B as in Example 2 in the present specification are used for the isomerization. The same procedure as in Example 2 is repeated except that operation temperature is 360°C to obtain oil P-A1. The decreasing ratio of a fraction having a boiling point of not lower than 360°C derived from analytical results of oil P-A1 by the

distillation gas chromatography is 45.4% by weight. The oil P-A1 is dewaxed in the same manner as Example 1 to obtain dewaxed oil DWO-A1. The fraction having a boiling point of not lower than 360°C is fractional-distilled from the dewaxed oil DWO-A1 through a TBP distillation apparatus to obtain lubricant base oil L-A1. The analytical results of the lubricant base oil L-A1 about the same items as in Example 1 are shown in Table A. The total content of normal paraffin and isoparaffin is 100% by weight.

(Additional Comparative Example A2)

The same starting wax B and catalyst B as in Comparative Example 2 in the present specification are used for the isomerization. The same procedure as in Comparative Example 2 is repeated except that LHSV is 0.44 hr⁻¹ and operation temperature is 350°C to obtain oil P-A2. The decreasing ratio of a fraction having a boiling point of not lower than 360°C derived from analytical results of oil P-A2 by the distillation gas chromatography is 30.9% by weight. The oil P-A2 is dewaxed in the same manner as Example 1 to obtain dewaxed oil DWO-A2. The fraction having a boiling point of not lower than 360°C is fractional-distilled from the dewaxed oil DWO-A2 through a TBP distillation apparatus to obtain lubricant base oil L-A2. The analytical results of the lubricant base oil L-A2 about the same items as in Example 1 are shown in Table A. The total content of normal paraffin and isoparaffin is 100% by weight.

(Additional Comparative Example A3)

The same starting wax B and catalyst B as in Comparative Example 2 in the present specification are used for the isomerization. The same procedure as in Comparative Example 2 is repeated except that LHSV is 0.44 hr⁻¹ and operation temperature is 340°C to obtain oil P-A3. The decreasing ratio of a fraction having a boiling point of not lower than 360°C derived from analytical results of oil P-A3 by the distillation gas chromatography is 14.3% by weight. The oil P-A3 is dewaxed in the same manner as Example 1 to obtain dewaxed oil DWO-A3. The fraction having a boiling point of not lower than 360°C is fractional-distilled from the dewaxed oil DWO-A3 through a TBP distillation apparatus to obtain lubricant base oil L-A3. The analytical results of the lubricant base oil L-A3 about the same items as in Example 1 are shown in Table A. The total content of normal paraffin and isoparaffin is 100% by weight.

(Additional Comparative Example A4)

The same starting wax B and catalyst B as in Comparative Example 2 in the present specification are used for the isomerization. The same procedure as in Comparative Example 2 is repeated except that operation temperature is 350°C to obtain oil P-A4. The decreasing ratio of a fraction having a boiling point of not lower than 360°C derived from analytical results of oil

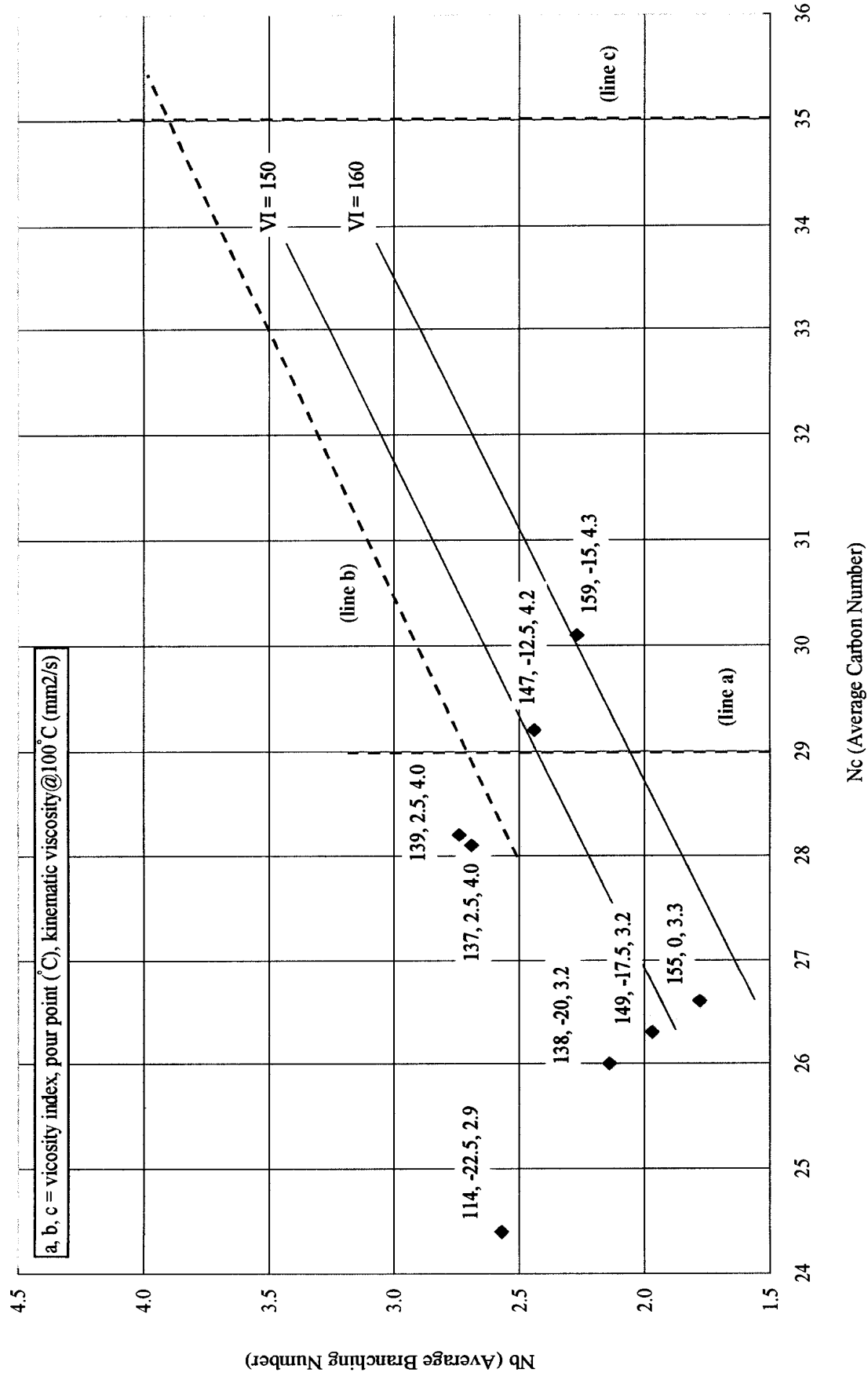
P-A4 by the distillation gas chromatography is 8.3% by weight. The oil P-A4 is dewaxed in the same manner as Example 1 to obtain dewaxed oil DWO-A4. The fraction having a boiling point of not lower than 360°C is fractional-distilled from the dewaxed oil DWO-A4 through a TBP distillation apparatus to obtain lubricant base oil L-A4. The analytical results of the lubricant base oil L-A4 about the same items as in Example 1 are shown in Table A. The total content of normal paraffin and isoparaffin is 100% by weight.

Furthermore, (1) the results obtained from the above additional Comparative Examples and (2) the results described in the original specification are summarized in the following Figure.

Table A

| | | Additional Comparative Example A1 | Additional Comparative Example A2 | Additional Comparative Example A3 | Additional Comparative Example A4 |
|---|--------------------|---|---|---|---|
| Lubricant base oil | | Lubricant base oil L-A1 | Lubricant base oil L-A2 | Lubricant base oil L-A3 | Lubricant base oil L-A4 |
| Kinematic Viscosity at 40°C | mm ² /s | 16.7 | 11.9 | 11.8 | 12.0 |
| Kinematic Viscosity at 100°C | mm ² /s | 4.0 | 3.2 | 3.2 | 3.3 |
| Viscosity index | – | 139 | 138 | 149 | 155 |
| Pour point | °C | 2.5 | -20 | -17.5 | 0 |
| Ratio of CH ₃ carbon from ¹³ C-NMR analysis | % | 16.7 | 15.9 | 15.1 | 14.2 |
| Ratio of CH ₂ carbon from ¹³ C-NMR analysis | % | 73.9 | 75.4 | 77.1 | 78.7 |
| Ratio of CH carbon from ¹³ C-NMR analysis | % | 9.4 | 8.7 | 7.8 | 7.2 |
| Average carbon number from distillation | number | 28.1 | 26.0 | 26.3 | 26.6 |
| Average branch number | number | 2.7 | 2.1 | 2.0 | 1.8 |
| Yield of lubricant base oil | wt% | 54.1 | 63.0 | 66.8 | 65.9 |

Figure. Molecular Structural Parameters and Properties as Lubricant Base Oils Prepared from FT waxes and α -olefins



Summary

As seen from the above Table A and Figure, there is a suitable range of Nb and Nc to maximize viscosity properties, especially viscosity index of the lubricant base oil composed mainly of isoparaffins. I firmly believe this finding will be a key technology for producing lubricant base oils of extremely high performance.

I declare further that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under § 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issuing thereon.

Date: April 13, 2010

Declarant: M. Kobayashi
Manabu Kobayashi